

# Dynamics of Systems

## CTB 2300

**Dr. Karel N. van Dalen**

**Dr. Hayo Hendrikse**

**Prof. Andrei V. Metrikine**

**Department:** Engineering Structures

**Research group:** Dynamics of Solids & Structures

**Room:** 3.61

**E-mail:** [K.N.vanDalen@tudelft.nl](mailto:K.N.vanDalen@tudelft.nl)

**Web:** [www.tudelft.nl/knvandalen](http://www.tudelft.nl/knvandalen)

**Department:** Hydraulic Engineering

**Research group:** Offshore Engineering

**Room:** 3.71

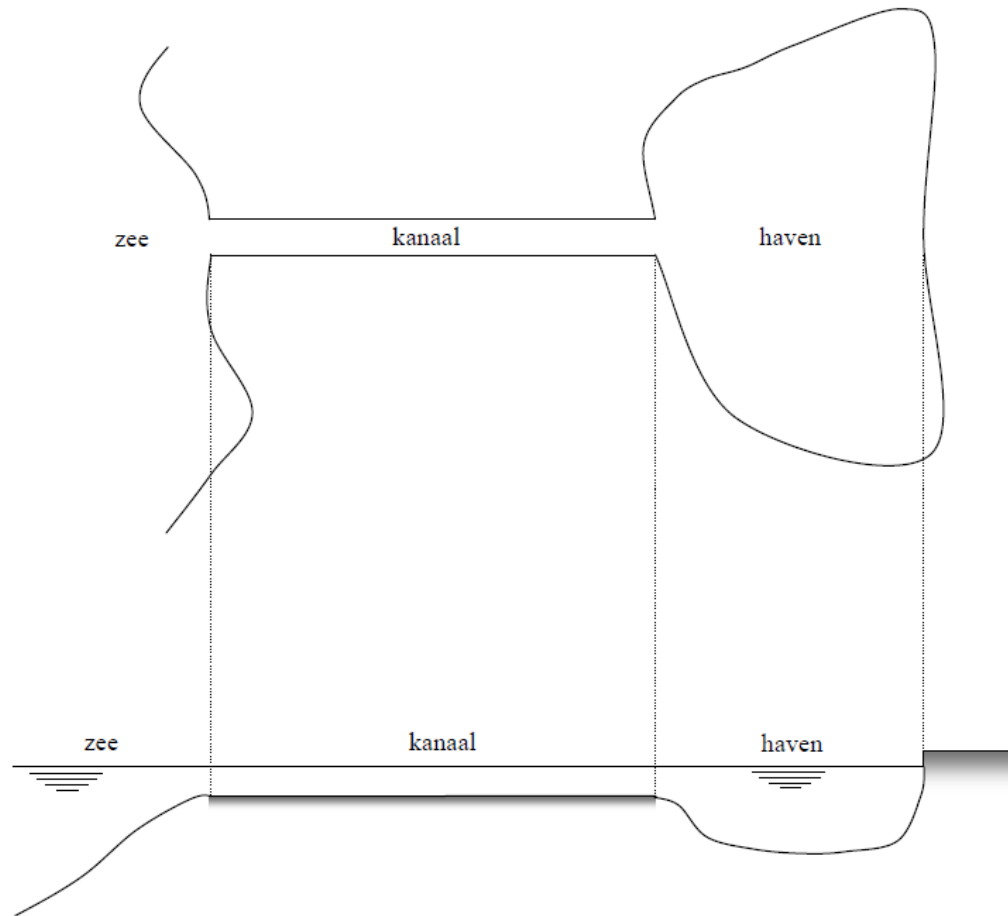
**E-mail:** [H.Hendrikse@tudelft.nl](mailto:H.Hendrikse@tudelft.nl)

**Web:** [tinyurl.com/hhendrikse](http://tinyurl.com/hhendrikse)

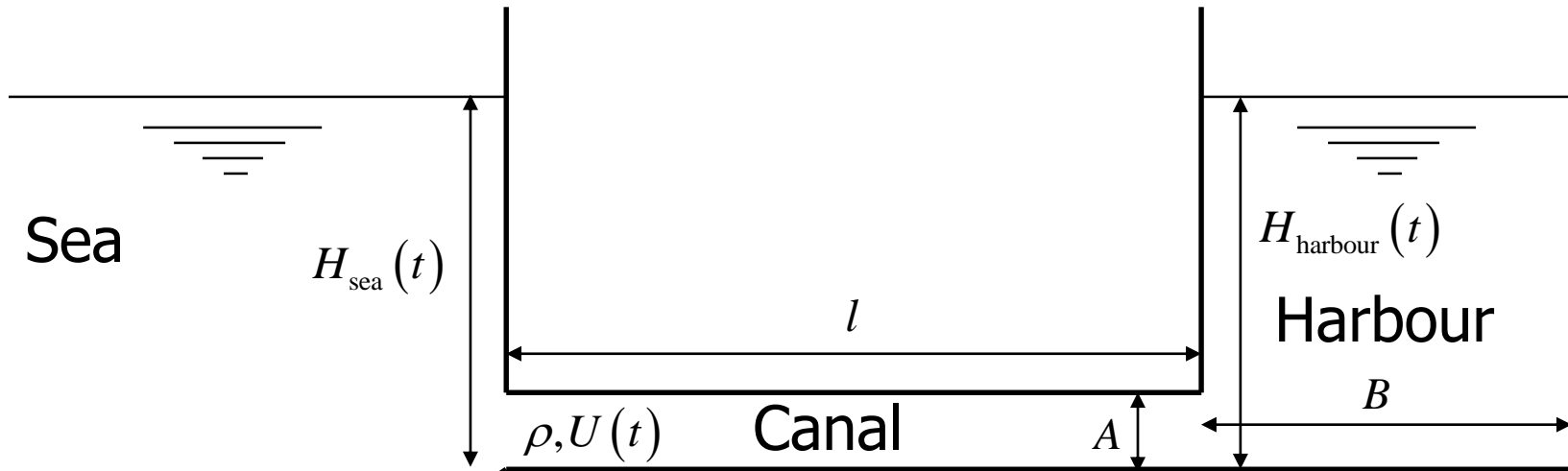
# Contents of Lecture 12

- 1. Equation of motion for the water level in a harbour connected with Sea by a canal**
- 2. Analogy with the mechanical oscillations**
- 3. Analysis of the hydraulic systems based on the solutions obtained for the mechanical systems**
- 4. Other examples of oscillatory dynamical systems**

# Dynamics of the water level in a harbour



# Dynamics of the water level in a harbour



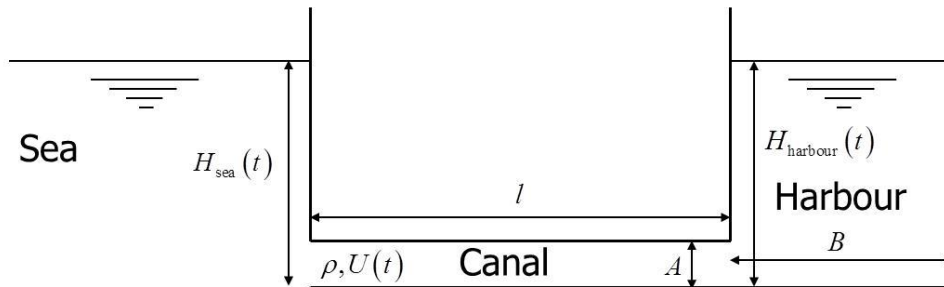
$$\frac{d(m_{\text{canal}}U)}{dt} = A(p_{\text{sea}} - p_{\text{harbour}})$$

$$\frac{d(m_{\text{harbour}})}{dt} = \rho AU$$

$$m_{\text{canal}} = \rho Al$$

$$m_{\text{harbour}} = \rho BH_{\text{harbour}}$$

# Dynamics of the water level in a harbour



$$\frac{d(m_{\text{canal}} U)}{dt} = A(p_{\text{sea}} - p_{\text{harbour}}) \Rightarrow m_{\text{canal}} \dot{U} = A(\rho g H_{\text{sea}} - \rho g H_{\text{harbour}})$$

$$\begin{cases} \frac{d(m_{\text{harbour}})}{dt} = \rho A U \\ m_{\text{harbour}} = \rho B H_{\text{harbour}} \end{cases} \Rightarrow \rho B \dot{H}_{\text{harbour}} = \rho A U \Rightarrow B \dot{H}_{\text{harbour}} = A U \Rightarrow U = \frac{B}{A} \dot{H}_{\text{harbour}}$$

$$\begin{cases} m_{\text{canal}} \dot{U} = A(\rho g H_{\text{sea}} - \rho g H_{\text{harbour}}) \\ m_{\text{canal}} = \rho A l \end{cases} \Rightarrow (\rho A l) \frac{B}{A} \ddot{H}_{\text{harbour}} = A(\rho g H_{\text{sea}} - \rho g H_{\text{harbour}})$$

# Dynamics of the water level in a harbour

$$(\rho Al) \frac{B}{A} \ddot{H}_{\text{harbour}} = A(\rho g H_{\text{sea}} - \rho g H_{\text{harbour}}) \Rightarrow \rho B l \ddot{H}_{\text{harbour}} + \rho A g H_{\text{harbour}} = \rho A g H_{\text{sea}}$$

$$\rho B \ddot{H}_{\text{harbour}} + \rho A \frac{g}{l} H_{\text{harbour}} = \rho A \frac{g}{l} H_{\text{sea}}$$

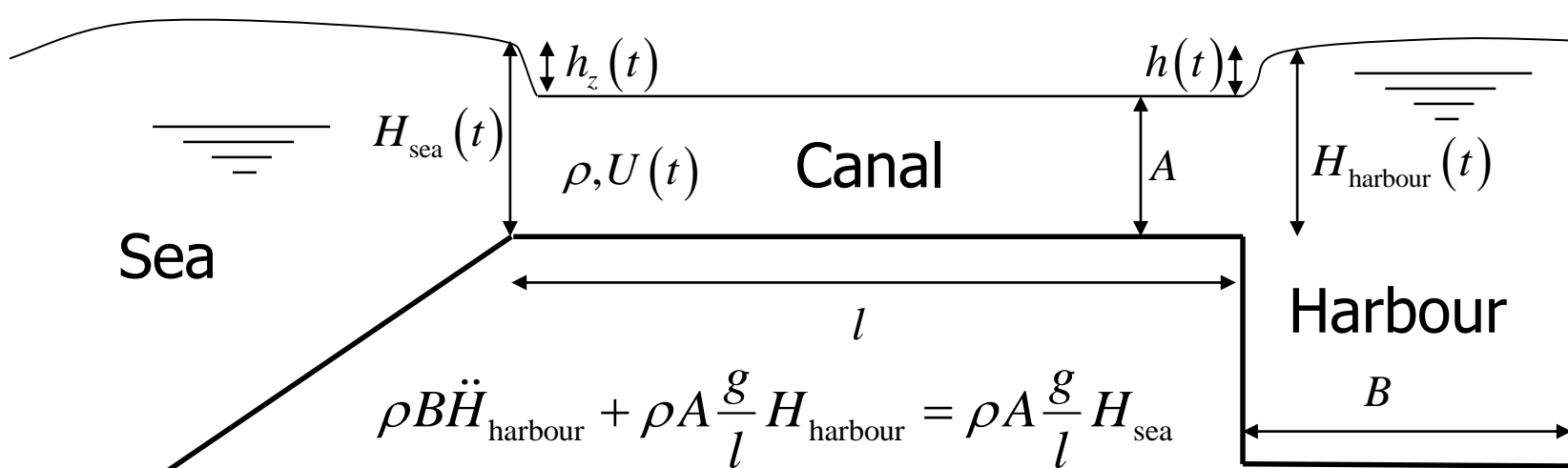
$\rho B$  - mass of water in the harbour per unit height

$\rho A \frac{g}{l}$  - force from the harbour on the water in the canal per unit height

(equivalent spring constant)

$\rho A \frac{g}{l}$  - force from the sea on the water in the canal per unit height

# Dynamics of the water level in a harbour



$$\rho B \ddot{H}_{\text{harbour}} + \rho A \frac{g}{l} H_{\text{harbour}} = \rho A \frac{g}{l} H_{\text{sea}}$$

$$H_{\text{harbour}} = A/b + h, \quad H_{\text{sea}} = A/b + h_z,$$

$b$  - width of the canal

$$\rho B \ddot{h} + \rho A \frac{g}{l} \left( \frac{A}{b} + h \right) = \rho A \frac{g}{l} \left( \frac{A}{b} + h_z \right)$$

$$\rho B \ddot{h} + \rho A \frac{g}{l} h = \rho A \frac{g}{l} h_z$$

# Analogy with the mass-spring system subject to a force

$$\rho B \ddot{h} + \rho A \frac{g}{l} h = \rho A \frac{g}{l} h_z \quad \text{Equations of motion} \quad m \ddot{u} + ku = F_u$$

---

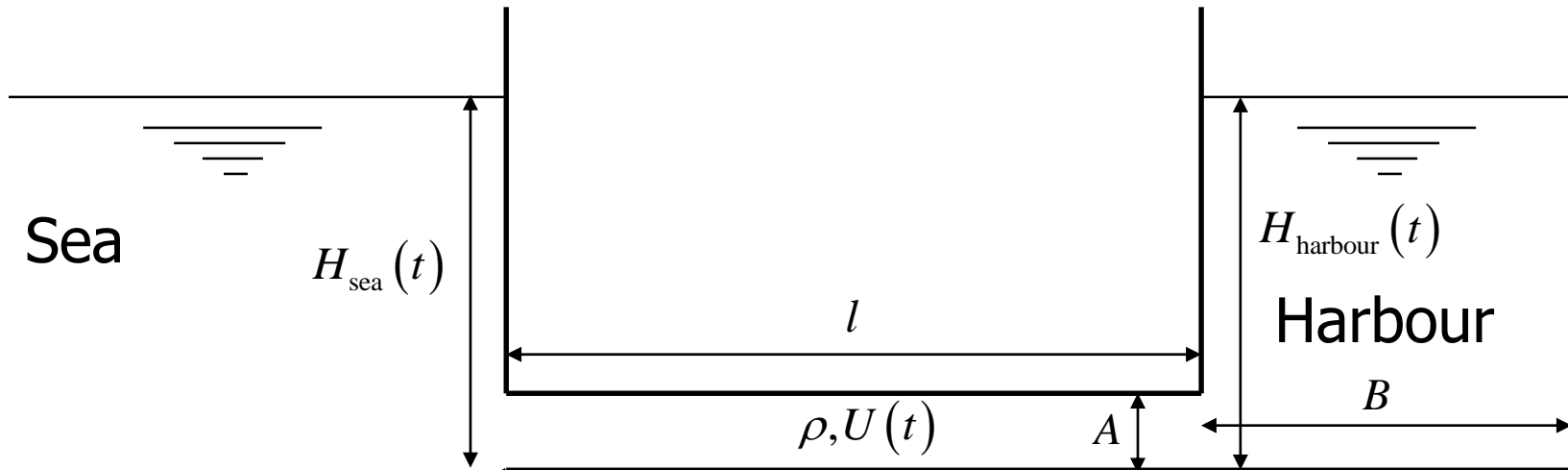
$$\rho B \leftrightarrow m \quad (\text{mass per unit height} \leftrightarrow \text{mass})$$

$$\rho A \frac{g}{l} \leftrightarrow k \quad (\text{equivalent stiffness} \leftrightarrow \text{stiffness})$$

$$\rho A \frac{g}{l} h_z \leftrightarrow F_u \quad (\text{force} \leftrightarrow \text{force})$$



# Effect of the friction with the canal bottom



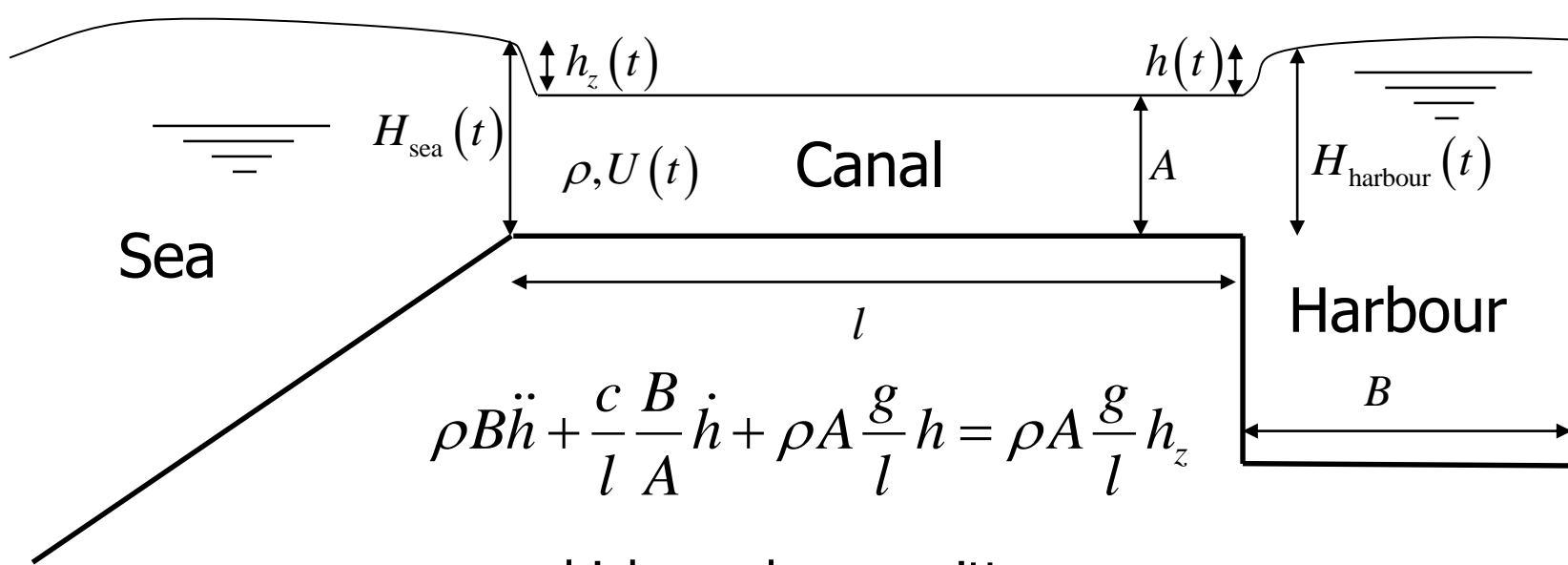
$$\frac{d(m_{\text{canal}} U)}{dt} = A(p_{\text{sea}} - p_{\text{harbour}}) - cU$$

$$\frac{d(m_{\text{harbour}})}{dt} = \rho AU$$

$$m_{\text{canal}} = \rho Al$$

$$m_{\text{harbour}} = \rho BH_{\text{harbour}}$$

# Effect of the friction with the canal bottom

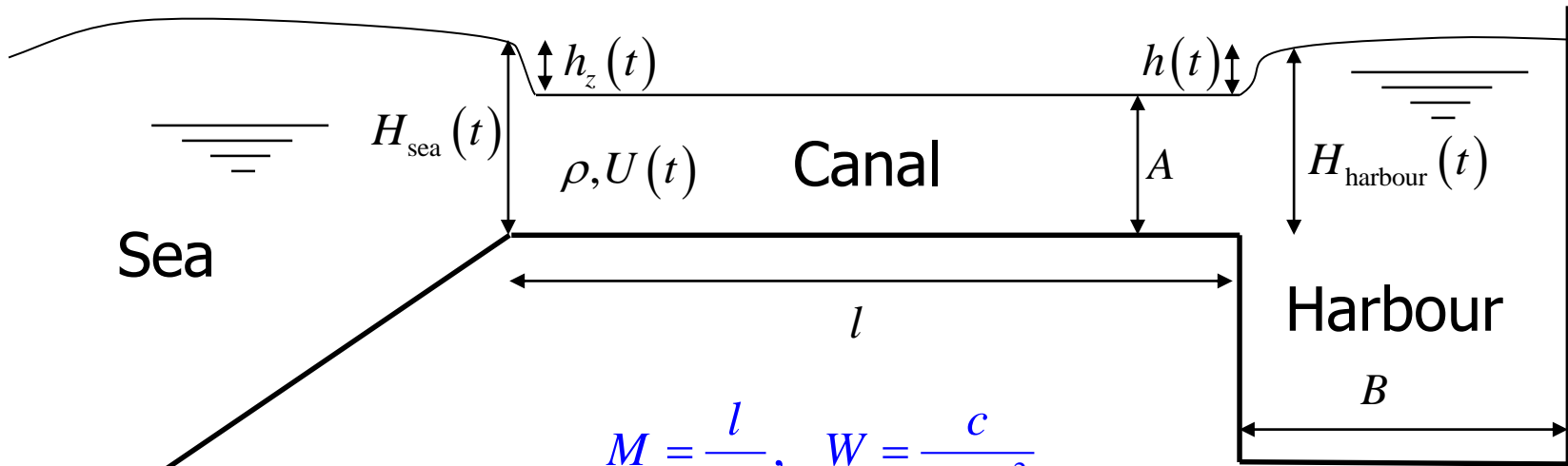


which can be re-written as

$$BM\ddot{h} + BW\dot{h} + h = h_z,$$

$$M = \frac{l}{gA}, \quad W = \frac{c}{\rho g A^2}$$

# Some specific hydraulic definitions



$$M = \frac{l}{gA}, \quad W = \frac{c}{\rho g A^2}$$

$$\begin{cases} \frac{d(m_{\text{canal}} U)}{dt} = A(p_{\text{sea}} - p_{\text{harbour}}) - cU \\ m_{\text{canal}} = \rho A l \end{cases}$$

$$\longrightarrow M\dot{Q} + WQ = h_z - h \quad (Q = AU)$$

$$\begin{cases} \frac{d(m_{\text{harbour}})}{dt} = \rho A U \\ m_{\text{harbour}} = \rho B H_{\text{harbour}} \end{cases}$$

$$\longrightarrow B\dot{h} = Q$$

$$BM\ddot{h} + BW\dot{h} + h = h_z$$

Lecture 12

Discharge (debiet):  $Q$

11

Inertia (traagheid):  $M$

# How to analyze?

$$BM\ddot{h} + BW\dot{h} + h = h_z$$



$$\ddot{h} + \frac{W}{M}\dot{h} + \frac{1}{BM}h = \frac{1}{BM}h_z$$



$$\ddot{h} + 2\zeta\omega_0\dot{h} + \omega_0^2h = f(t)$$

$$\omega_0^2 = \frac{1}{BM}, \quad \zeta = \frac{W}{2} \sqrt{\frac{B}{M}}, \quad f(t) = \frac{h_z(t)}{BM}$$

# We can simply use all formulas obtained for the mass-spring-dashpot system

$$\ddot{h} + 2\zeta\omega_0\dot{h} + \omega_0^2 h = f(t)$$

$$\omega_0^2 = \frac{1}{BM}$$

$$\zeta = \frac{W}{2} \sqrt{\frac{B}{M}}$$

$$f(t) = \frac{h_z(t)}{BM}$$

hydraulic system

$$\ddot{u} + 2\zeta\omega_0\dot{u} + \omega_0^2 u = f(t)$$

$$\omega_0^2 = \frac{k}{m}$$

$$\zeta = \frac{c}{2\sqrt{km}}$$

$$f(t) = \frac{F(t)}{m}$$

mechanical system

## Example 1: free vibration of the hydraulic system

As derived in Lecture 6, slide 19, the sub-critically damped free vibration of a mechanical system is described by

$$u(t) = \exp(-\zeta\omega_0 t) \left( u_0 \cos(\omega_1 t) + \frac{v_0 + \zeta\omega_0 u_0}{\omega_1} \sin(\omega_1 t) \right)$$

Therefore, using the expressions given on the previous slide, we find the following expression for the hydraulic system

$$h(t) = \exp(-\zeta\omega_0 t) \left( h(0) \cos(\omega_1 t) + \frac{\dot{h}(0) + \zeta\omega_0 h(0)}{\omega_1} \sin(\omega_1 t) \right)$$

$$\omega_0^2 = \frac{1}{BM}, \quad \zeta = \frac{W}{2} \sqrt{\frac{B}{M}}, \quad \omega_1 = \omega_0 \sqrt{1 - \zeta^2} = \frac{1}{\sqrt{BM}} \sqrt{1 - \frac{W^2}{4} \frac{B}{M}}$$

## Example 2: amplitude of the steady-state vibration of the hydraulic system caused by $h_z(t) = h_{z0} \cos(\omega t)$

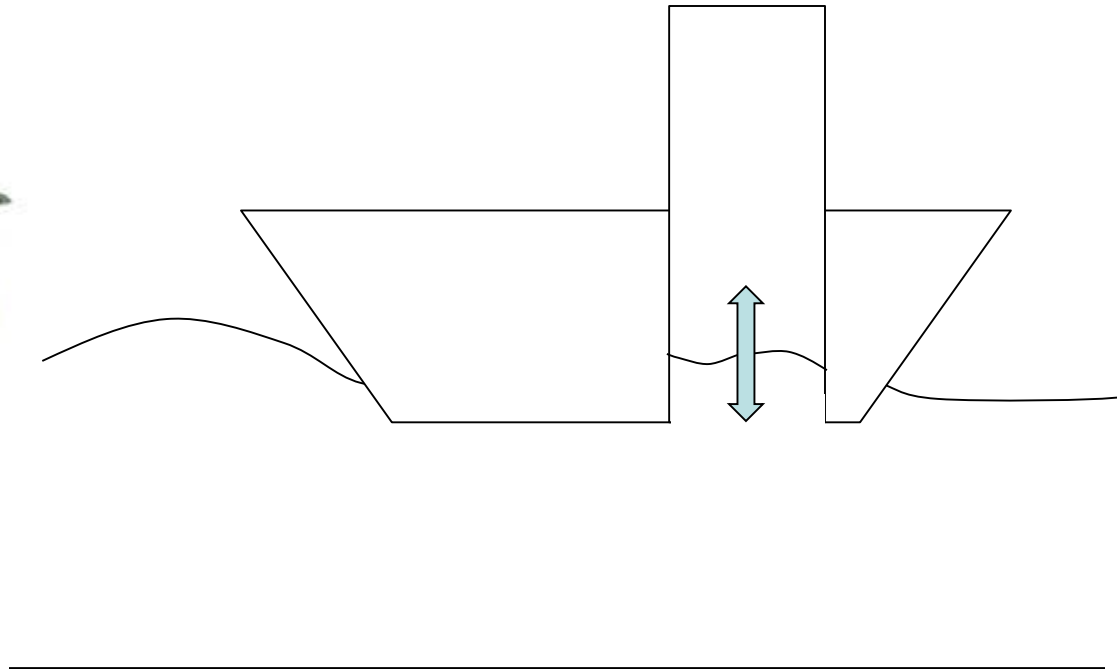
As derived in Lecture 7, slide 11, the amplitude of the steady-state response of the corresponding mechanical system is given as

$$U_{\text{steady}} = \frac{u_{\text{static}}}{\sqrt{\left(1 - \omega^2/\omega_0^2\right)^2 + 4\zeta^2 \omega^2/\omega_0^2}}, \quad u_{\text{static}} = \frac{F_0}{k} = \frac{f_0}{\omega_0^2}$$

Therefore, using the relevant expressions for the hydraulic system (slide 13 of the current lecture), we obtain

$$H_{\text{steady}} = \frac{f_0}{\omega_0^2} \frac{1}{\sqrt{\left(1 - \omega^2/\omega_0^2\right)^2 + 4\zeta^2 \omega^2/\omega_0^2}}$$
$$\omega_0^2 = \frac{1}{BM}, \quad \zeta = \frac{W}{2} \sqrt{\frac{B}{M}}, \quad f_0 = \frac{h_{z0}}{BM}$$

# Other examples of SDOF dynamical systems: pressure fluctuations in an enclosed moonpool of an arctic drillship





# Other examples of SDOF dynamical systems: the Helmholtz resonator (sound trapper)



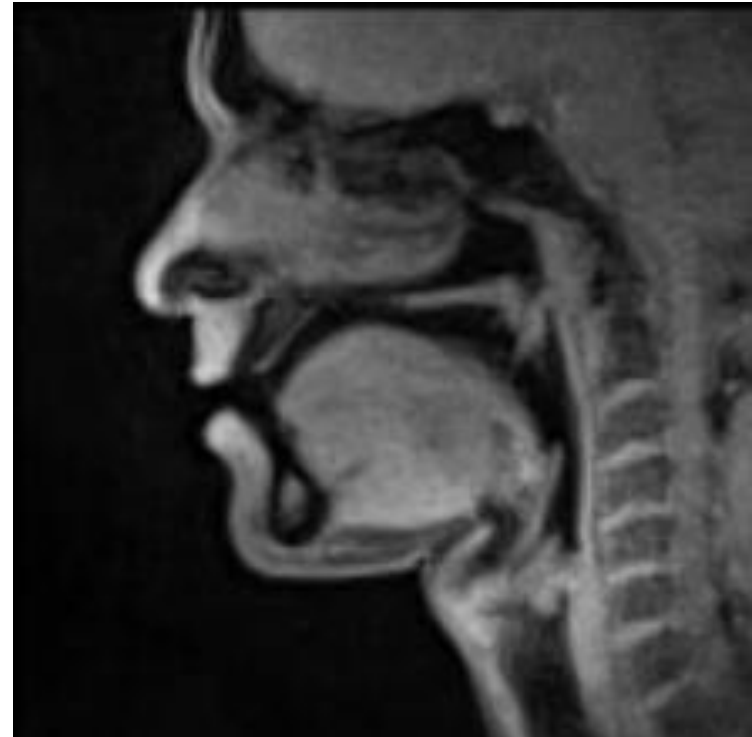
$$\omega_0 = c_{\text{sound}} \sqrt{\frac{A}{V_0 L}}$$



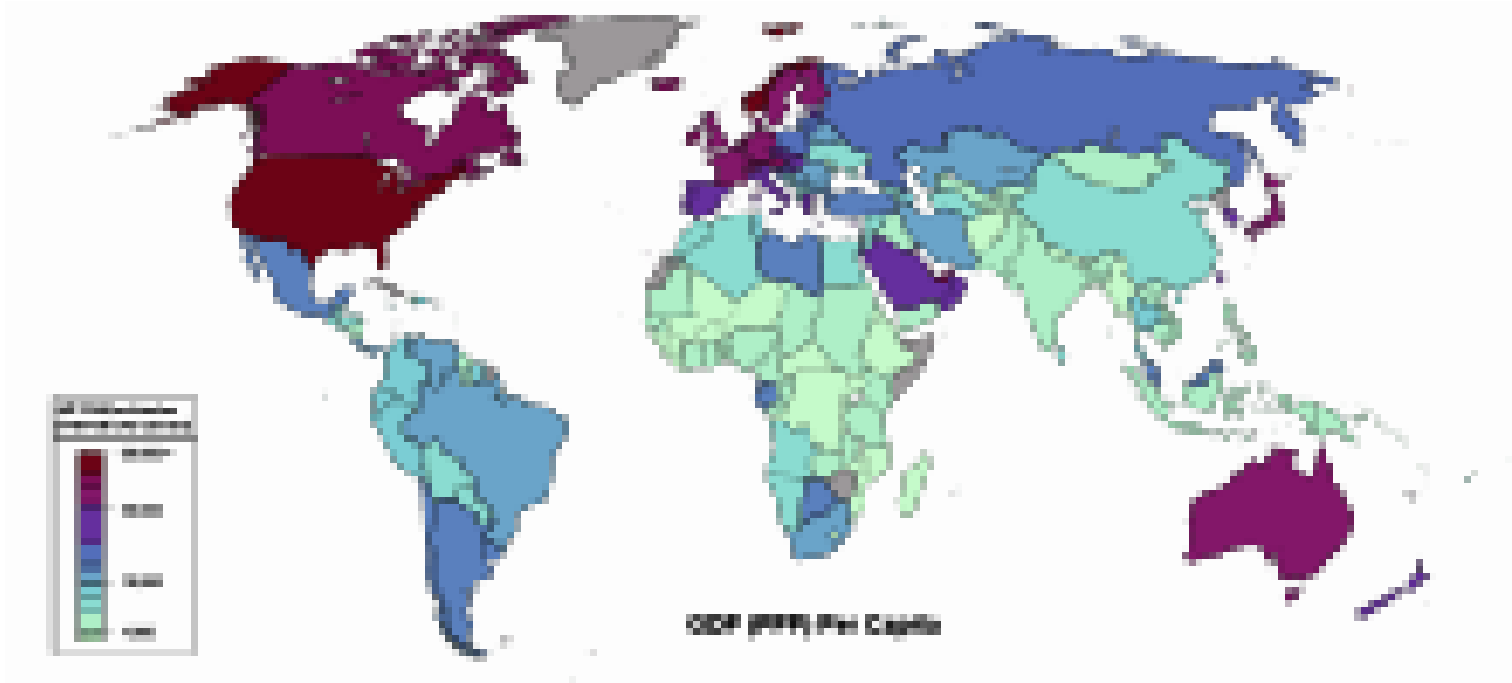
# Other examples of SDOF dynamical systems: a loudspeaker



# Other examples of SDOF dynamical systems: voice production



# Other examples of SDOF dynamical systems: business cycle



## Other examples of SDOF dynamical systems: predator-pray interaction

$$\dot{x} = bx - pxy \quad (\text{pray})$$



$x(t)$  – Number of the prays (rabbits)

$$\dot{y} = -dy + rxy \quad (\text{predator})$$



$y(t)$  – Number of the predators (foxes)